

3 INPhO-2008

1. Note that

A : has dimensions of energy.

B : has dimensions of length.

C : is dimensionless.

Now the Bohr radius will have a combination of B and C .

$$r_n = \frac{n^2 B}{2\pi C}$$

The energy will have a combination of A and C .

$$E_n = -\frac{1}{2n^2} AC^2$$

The Rydberg constant (of dimensions length inverse) will have a combination of B^{-1} and C .

$$R = \frac{C^2}{2B}$$

Note: This problem can be done in number of ways.

2.

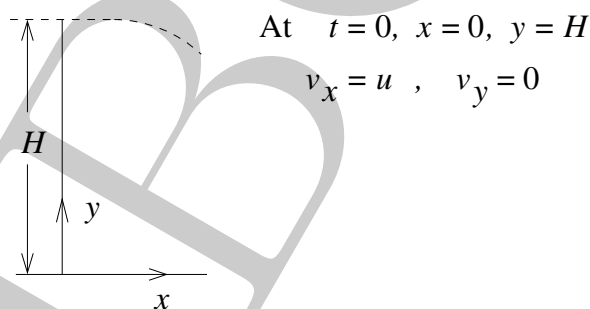


Figure 18: Problem 2 (a)

(a) See Fig.(18)

$$\begin{aligned} \frac{dv_x}{dt} &= -cv_x \\ x &= \frac{u}{c} (1 - e^{-ct}) \end{aligned} \quad (39)$$

$$\begin{aligned} \frac{dv_y}{dt} &= -g - cv_y \\ \frac{dy}{dt} &= -\frac{g}{c} (e^{-ct} - 1) \end{aligned}$$

and
$$y = H + \frac{g}{c^2} - \frac{g}{c} \left[\frac{1}{c} e^{-ct} + t \right] \quad (40)$$

(b) From Eq. (39)

$$t = -\frac{1}{c} \ln \left(1 - \frac{xc}{u} \right)$$

Substituting in Eq. (40),

$$y = H + \frac{g}{c^2} - \frac{g}{c} \left[\frac{1}{c} e^{\ln \left(1 - \frac{xc}{u} \right)} - \frac{1}{c} \ln \left(1 - \frac{xc}{u} \right) \right]$$

$$y = H + \frac{g}{c^2} - \frac{g}{c^2} \left(1 - \frac{xc}{u} \right) + \frac{g}{c^2} \ln \left(1 - \frac{xc}{u} \right)$$

$$y = H + \frac{gx}{cu} + \frac{g}{c^2} \ln \left(1 - \frac{xc}{u} \right)$$

If c is small and the range is limited, e.g. $\frac{xc}{u} \ll 1$ then

$$y = H + \frac{gx}{cu} + \frac{g}{c^2} \left[-\frac{xc}{u} - \frac{x^2 c^2}{2u^2} - \frac{x^3 c^3}{3u^3} + \dots \right] \quad (41)$$

$$y = H - \frac{g x^2}{2u^2} - \frac{g x^3 c}{3u^3}$$

- (c) The trajectory is foreshortened (see Fig. (19)).
Note $c = 0$ is without air resistance
and $c \neq 0$ is with air resistance.

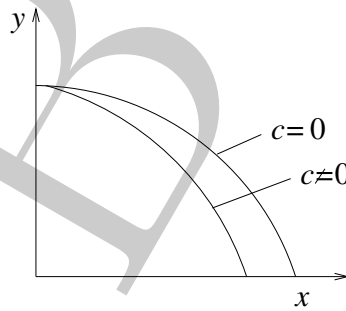


Figure 19: Problem 2 (c)

(d) When $y = 0$, from Eq. (40)

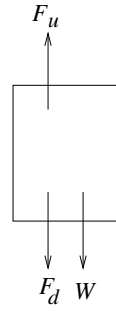
$$H + \frac{g}{c^2} [1 - e^{-ct} - ct] = 0$$

$$\text{For } H = 500 \text{ m, } c = 0.05 \text{ s}^{-1}, \quad g = 10 \text{ m} \cdot \text{s}^{-2}$$

$$t = 10 + 1.1 = 11.1 \text{ s}$$

The above answer is obtained by iterative analysis. You may verify that the approximation in Eq. (41) is valid.

3. (a) Free Body Diagram, see Fig. (20)



F_u = Upward tension due to upper part

F_d = Downward tension due to lower part

W = Weight

Figure 20: Problem 3 (a)

(b)

$$F_U - F_D = W - F_C$$

$$A(dT) = \frac{GM\rho A dr}{r^2} - \omega^2 r \rho A dr$$

$$\frac{dT}{dr} = GM\rho \left[\frac{1}{r^2} - \frac{r}{R_g^3} \right] \quad (\text{using Kepler's third law}) \quad (42)$$

(c) Integrating Eq. (42)

$$\begin{aligned} \int_a^b dT &= \int GM\rho \left(\frac{1}{r^2} - \frac{r}{R_g^3} \right) dr \\ T_b - T_a &= GM\rho \left[-\frac{1}{r} - \frac{r^2}{2R_g^3} \right] \Big|_a^b \end{aligned} \quad (43)$$

For $r \rightarrow R_g$ and $T(R) = 0$

$$T(R_g) = GM\rho \left[-\frac{3}{2R_g} + \frac{R^2}{2R_g^3} + \frac{1}{R} \right] \quad (44)$$

For $r \rightarrow R_g$ and $T(H) = 0$

$$T(R_g) = GM\rho \left[-\frac{3}{2R_g} + \frac{H^2}{2R_g^3} + \frac{1}{H} \right] \quad (45)$$

Equating Eqs. (44) and (45) we obtain

$$\begin{aligned} H &= \frac{R}{2} \left[\sqrt{1 + \frac{8R_g^3}{R^3}} - 1 \right] \\ &= 1.51 \times 10^5 \text{ km} \end{aligned}$$

(d) See Fig. (21)

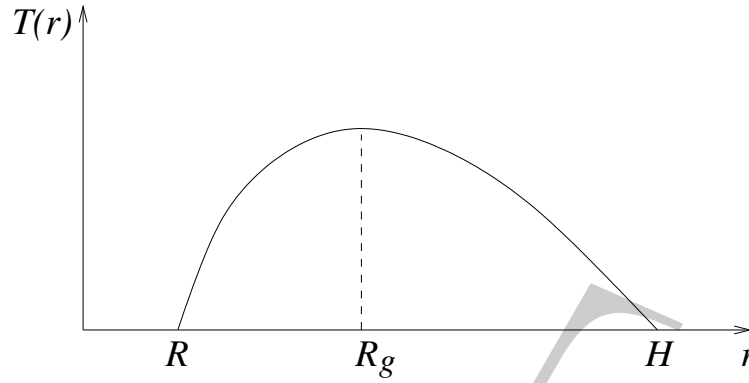


Figure 21: Problem 3 (d)

- (e) Maximum stress will be at $r = R_g$
Using Eq. (44)

$$T(R_g) = 379 \text{ GPa}$$

Steel has tensile strength 6.37 GPa which is less than 379 GPa. Hence it will not be feasible.

4.

$$T_0 = \frac{T_1 + T_2}{2}, \Delta = T_2 - T_1, \delta = T'' - T'$$

$$T_1 = 270\text{K}, T_2 = 298\text{K}$$

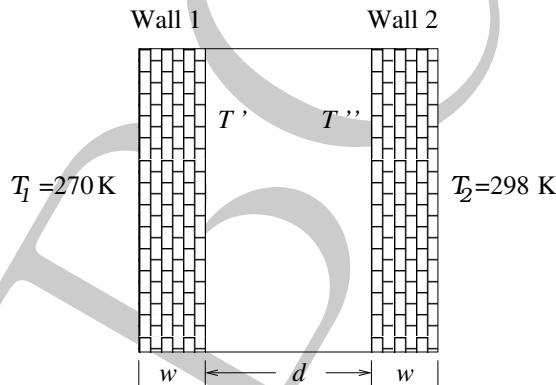


Figure 22: Problem 4

- (a) For wall 1, $q_w = \frac{k_w}{w} (T_2 - T'')$
For wall 2, $q_w = \frac{k_w}{w} (T' - T_1)$

(b)

$$\Delta - \delta = T_2 - T'' + T' - T_1$$

For stationary process,

$$T_2 - T'' = T' - T_1 \quad (46)$$

$$\Delta - \delta = 2(T_2 - T'')$$

Hence,

$$q_w = \frac{k_w}{w} \frac{(\Delta - \delta)}{2}$$

(c)

$$E_1 = \epsilon \sigma T'^4 + (1 - \epsilon) E_2$$

and

$$E_2 = \epsilon \sigma T''^4 + (1 - \epsilon) E_1$$

$$\begin{aligned} q_r &= E_2 - E_1 \\ &= \frac{\epsilon \sigma}{(2 - \epsilon)} (T''^4 - T'^4) \end{aligned}$$

(d) Using Eq. (46) and given set of equations,

$$T'' = T_0 + \frac{\delta}{2}, \quad T' = T_0 - \frac{\delta}{2} \quad (47)$$

also,

$$\begin{aligned} T''^4 - T'^4 &= (T''^2 - T'^2)(T''^2 + T'^2) \\ &= 2\delta T_0 [(T'' + T')^2 - 2T'' T'] \end{aligned}$$

putting values from Eq. (47)

$$= 4\delta T_0^3 \left[1 + \left(\frac{\delta}{2T_0} \right)^2 \right]$$

again, $q_r = q_w$

$$\frac{\epsilon \sigma}{(2 - \epsilon)} (T''^4 - T'^4) = \frac{k_w}{w} \frac{(\Delta - \delta)}{2}$$

since, $(\delta^2 \ll T_0^2)$

$$\frac{\epsilon \sigma}{(2 - \epsilon)} 4\delta T_0^3 = \frac{k_w}{w} \frac{(\Delta - \delta)}{2}$$

$$1 - \frac{\delta}{\Delta} = 8c T_0^3 \frac{\delta}{\Delta}$$

where,

$$c = \frac{\sigma \epsilon w}{k_w (2 - \epsilon)}$$

$$\delta = \frac{\Delta}{1 + 8c T_0^3}$$

Now,

$$q_r = q_w = \frac{k_w}{w} \frac{(\Delta - \delta)}{2} = \frac{k_w}{w} \left(\frac{\Delta}{2} \frac{8c T_0^3}{1 + 8c T_0^3} \right)$$

(e)

$$c = 6.44 \times 10^{-10}, \quad w = 0.01 \text{ m}, \quad k_w = 0.72 \text{ W} \cdot \text{m}^{-1} \cdot \text{K}^{-1}$$

$$T_0 = 284 \text{ K}, \quad \Delta = 28 \text{ K}$$

$$q_r = 107.22 \text{ W} \cdot \text{m}^{-2}$$

(f)

$$q_{cv} = \frac{N_u K_a}{d} (T'' - T') = \frac{N_u K_a}{d} \delta$$

$$q_{cv} = q_w$$

gives,

$$\delta = \frac{\Delta}{1 + \frac{2w k_a N_u}{k_w d}}$$

$$q_{cv} = \frac{N_u k_a \Delta k_w}{k_w d + 2w k_a N_u}$$

(g) Ignoring $2w k_a N_u$
 $q_{cv} \simeq 46.5 \text{ W}\cdot\text{m}^{-2}$

(h)

$$q_{cd} = \frac{k_s}{d} (T'' - T') = \frac{k_s \delta}{d}$$

$$q_{cd} = q_w$$

From part (b),

$$\frac{k_w}{2w} (\Delta - \delta) = \frac{k_s \delta}{d}$$

which gives,

$$\delta = \frac{k_w \Delta d}{2w k_s + k_w d}$$

Hence,

$$q_{cd} = \frac{k_s k_w \Delta}{2w k_s + k_w d}$$

(i) $k_s = 0.05 \text{ W}\cdot\text{m}^{-1}\text{K}^{-1}$, $k_w = 0.72 \text{ W}\cdot\text{m}^{-2}$
 $w = 0.01 \text{ m}$, $d = 0.1 \text{ m}$
 $q_{cd} = 13.8 \text{ W}\cdot\text{m}^{-2}$

(j) Since,

$$q_{cd} < q_{cv} < q_r$$

Hence sheathing material is best for insulation.

5. See the brief solution.

6. (a) The force on one capacitor plate due to the other is

$$F_e = \frac{Q_1^2}{2A\epsilon_0}$$

$$F_e = \frac{C_1^2 V_0^2 \cos^2(2\pi ft)}{2\pi a^2 \epsilon_0}$$

Time - averaged force is

$$\langle F_e \rangle = \frac{C_1^2 V_0^2}{4\pi \epsilon_0 a^2} \quad (48)$$

(b) Charge on Capacitor C_2 : $Q_2 = C_2 V_0 \cos(2\pi f t)$

$$i_2 = -C_2 V_0 2\pi f \sin(2\pi f t)$$

(note: wire has negligible resistance.)

Force on one ring due to the other

$$F_m = i_2 l B$$

Hence,

$$F_m = \frac{\mu_0 b}{h} (-C_2 V_0 2\pi f \sin(2\pi f t))^2$$

Time- averaged force is

$$\langle F_m \rangle = \frac{\mu_0 b}{2h} C_2^2 V_0^2 (2\pi f)^2 \quad (49)$$

(c) Equating Eqs. (48) and (49)

$$\langle F_e \rangle = \langle F_m \rangle$$

$$\text{and noting } c^2 = \frac{1}{\mu_0 \epsilon_0}$$

We obtain

$$c = (2\pi)^{3/2} a \left(\frac{b}{h} \right)^{1/2} \frac{C_2}{C_1} f \quad (50)$$

(d) From Eq. (50) and given constants.

$$c = 2.99 \times 10^8 \text{ m}\cdot\text{s}^{-1}$$

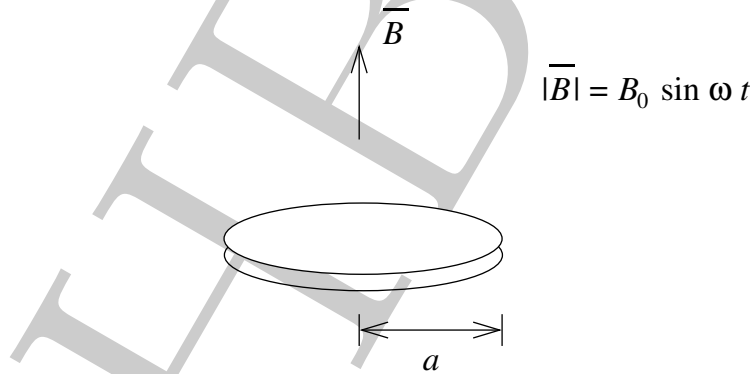


Figure 23: Problem 7

7. (a) Flux : $\phi = B_0 \sin(\omega t) \pi a^2 N$

$$\varepsilon = -\frac{d\phi}{dt} = -N\pi a^2 B_0 \omega \cos \omega t$$

From Kirchhoff's Law,

$$i R + L \frac{di}{dt} = -N\pi a^2 B_0 \omega \cos \omega t \quad (51)$$

- (b) Take $i = Rl(i_0 e^{j\omega t})$ ($j^2 = -1$)

Substituting the complex form in Eq. (51), we obtain,

$$i_0 = \frac{N \pi a^2 B_0 \omega (R - j\omega L)}{R^2 + \omega^2 L^2}$$

This implies,

$$i = \frac{N \pi a^2 B_0 \omega (R \cos \omega t + \omega L \sin \omega t)}{R^2 + \omega^2 L^2}$$

- (c) The elemental force

$$d\vec{F} = i d\vec{l} \times \vec{B}$$

is directed radially in. Substituting,

$$\frac{dF}{dl} = -\frac{NB_0^2 \pi a^2 \omega}{R^2 + \omega^2 L^2} (R \sin \omega t \cos \omega t + \omega L \sin^2 \omega t)$$

Time - averaged compressional force

$$\left. \frac{dF}{dl} \right|_{av} = -\frac{NB_0^2 \pi a^2 \omega^2 L}{2(R^2 + \omega^2 L^2)} \quad (52)$$

$$\left. \frac{dF}{dl} \right|_{osc} = -\frac{NB_0^2 \pi a^2 \omega}{2(R^2 + \omega^2 L^2)} (R \sin 2\omega t - \omega L \cos 2\omega t) \quad (53)$$

Net force on ring is zero by symmetry.

- (d) From Eq. (52)

$$\begin{aligned} \left. \frac{dF}{dl} \right|_{av} &= -\frac{\pi(10^{-2}) 10^6 10^{-1}}{2(10^2 + 10^4)} \\ &\simeq -\frac{\pi}{2} 10^{-1} N \\ &= 1.55 \text{ N}\cdot\text{m}^{-1} \end{aligned}$$

- (e) i. From Eq. (53) the oscillating force has a frequency of 2ω and hence the frequency of the sound is 120 Hz.
 ii. The inclusion of the capacitor will result in

$$\omega L \rightarrow \omega L - \frac{1}{\omega C}$$
 $\therefore$ the compressional force is lessened and may even become negative, i.e. tensile and outward.